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Assessment of carbon emissions' effects on the investments in conventional and innovative waste-to-energy treatments

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Best wishes,

Prof. Francesco Facchini (on behalf of all manuscripts' Authors)

1 **Assessment of carbon emissions' effects on the investments in conventional and** 2 **innovative Waste-to-Energy treatments**

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10

11 **Abstract:** In the current scenario of transition to a Europe-wide circular economy (CE), the Waste-to-Energy
12 (WtE) treatments represent a smart solution to generate renewable energy, reduce landfills and ensure
13 sustainable waste management. The costs and environmental impacts of existing WtE treatments are very
14 different for each available technology. In many cases, their identification is affected by a set of variable
15 boundary conditions strongly dependent on local municipal requirements. In light of these considerations,
16 the paper aims to compare the investment in three different WtE treatments (i.e., incineration, gasification,
17 and *flameless* oxy-combustion) to identify the best solution to support the current transitional phase towards
18 a CE condition. An overall yearly cost analysis was developed by varying local municipal requirements,
19 including investment, operating, and carbon emissions costs. The overall yearly cost and the revenues, due
20 to energy sales and tipping fees, allowed to evaluate the profitability of the investment in the plant lifetime
21 to identify the best WtE treatment. The investment profitability was evaluated by adopting the Net Present
22 Value (NPV) method by estimating the cash flow statement over the entire plant lifetime. The performance
23 of the three WtE treatments, classified as "conventional" (i.e., gasification and incineration) and "innovative"
24 (i.e., flameless oxy-combustion), were compared in a case study concerning Southern Italy's Metropolitan
25 City of Bari. The applied methodology showed, in this case, that gasification, at the moment, has to be
26 deemed as the most sustainable treatment for MSW management. Moreover, the study proved a high
27 dependence between the carbon price and the profitability of the investment and, thus, in the next future
28 the innovative oxy-combustion technology will gain an advantage over all the other technologies, when
29 carbon price will be higher than 44 €/tonnes_{CO2}.

30

31 **Keywords:** Circular economy, Economic and Environmental assessment, Municipal solid waste; Waste to
32 Energy, gasification, incineration, smart city.

33

34 List of abbreviations

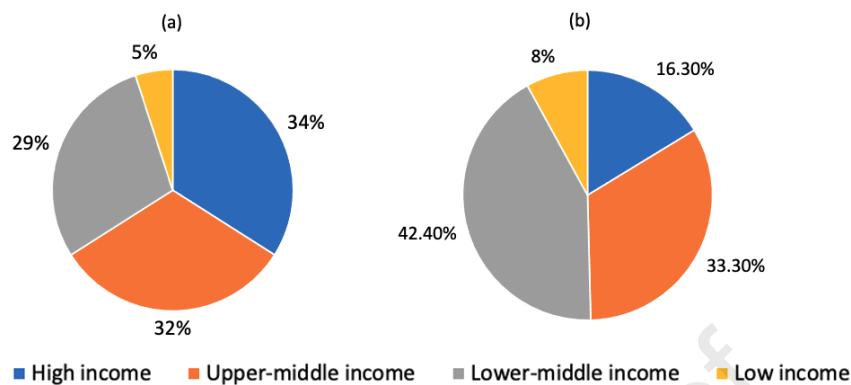
Notation	Meaning	Unit of measurement
$r_{t\ fee}$	Revenue from tipping fee payment	[€]
c_{cons}	Consumables cost	[€/tonne]
c_{em}	CO ₂ emissions cost	[€/tonne _{MSW}]
C_{ext}	Investment cost for plant size extension	[€/year]
C_{inv}	Annual investment cost	[€/year]
c_{lab}	Labour cost	[€/tonne _{MSW}]
C_m	Maintenance cost	[€/year]
c_{sbp}	Solid by-product disposal cost	[€/tonne]
p_{cons}	Consumables price	[€/tonne]
p_e	Price of the market for selling electricity	[€/MWh]
p_{em}	Price due to CO ₂ emissions	[€/tonne _{CO2}]
p_{sbp}	Price for disposing of solid by-products	[€/tonne]
q_{cons}	Amount of consumables required to treat 1t of MSW	[tonnes]
q_e	Amount of electricity produced by treating 1t of MSW	[MWh/tonne _{MSW}]
q_{em}	Amount of CO ₂ emitted to the air by treating one tonne of MSW	[tonnes _{CO2} / tonne _{MSW}]
Q_{std}	Plant standard size	[tonne _{MSW} /y]
r_e	Revenue from electricity sale	[€]
t_{fee}	Tipping fee	[€/tonne _{MSW}]
CCF	Cumulative Cash Flow	[-]
CDCF	Cumulative Discounted Cash Flow	[-]
CE	Circular Economy	[-]
CF	Cash Flow	[-]
DCF	Discounted Cash Flow	[-]
k	Scale coefficient	[-]
LCA	Life Cycle Assessment	[-]
LHV	Low Heating Value	[-]
MSW	Municipal Solid Waste	[-]
VLSFO	Very Low Sulfur Fuel Oil	[-]
WFD	Waste Framework Directive	[-]
WtE	Waste-to-energy	[-]

35
36

37 1. Introduction

38 The current increase in MSW production is a direct consequence of population growth (at a yearly rate of
39 2.035% [1]), which is accelerating phenomena such as industrialization, urbanization, and economic
40 development [1] [2]. The global production of MSW, equal to 2.01 billion tonnes in 2016, will grow to 2.56
41 billion in 2030 and will reach a level of 3.4 billion in 2050. As far as concern the correlation between MSW
42 production and economic development, in 2016, about 34% (683 million tonnes) of the globally produced
43 MSW was generated by high-income countries (i.e., countries with a gross national income per capita of

44 12,476 \$/year or more), despite the same countries being populated by only the 16% of the global
 45 population (Figure 1) [2].

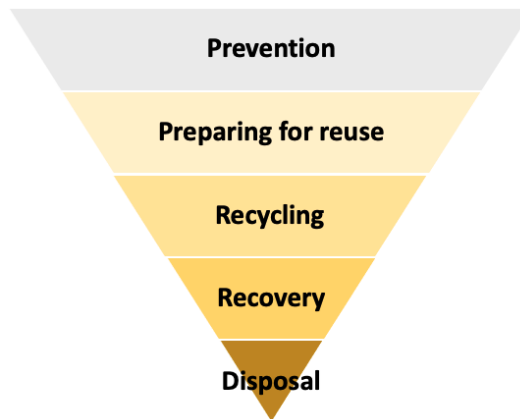


46

47 **Figure 1.** (a) Share of MSW produced globally in 2016 per income category. Adapted from [2]. (b) Share of the global population
 48 in 2016 per income category. Adapted from [3]

49 MSW management shows criticalities both from an economic and an environmental perspective. MSW,
 50 indeed, represents one of the most significant sources of pollution at either a global, regional, or local scale
 51 [4]. To this concern, in 2016, the MSW management practices generated 5% of the globally emitted 1.6
 52 billion tonnes of CO_{2eq} [2]. Furthermore, at a local and regional scale, the MSW management (e.g.,
 53 collection, transport, treatment, and disposal) is generally operated in proximity to the urban centres,
 54 representing a significant pollution source, very close to citizenship.

55 From an economic point of view, MSW management is an expensive service for municipalities; in high-
 56 income countries, it accounts for 4% of the municipal budget, and of this expenditure, operating costs
 57 represent about 70% [3]. Therefore, identifying a solution to manage the increasing amount of MSW
 58 produced, accounting for both economic and environmental issues, is a worldwide highly perceived need.
 59 The EU-27 countries are significantly involved in this issue since most of them are included in the high-
 60 income category (Figure 1). Several legislative measures have been enacted in the EU to promote
 61 sustainable MSW management. The most impactful is the Waste Framework Directive (WFD) 2008/98/EC
 62 [5], which can be considered the cornerstone of the European waste policy and regulation. The WFD
 63 introduced a waste hierarchy describing, in descending order of priority, the actions to be implemented to
 64 manage waste in an environmentally sustainable way, optimising resource efficiency and minimising the
 65 environmental consequences of waste management (Figure 2) [6].

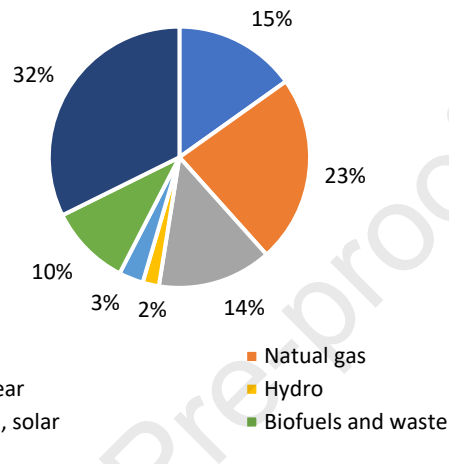


66
67 **Figure 2.** Waste hierarchy pyramid. Adapted from [6]

68 According to the WFD, sustainable waste management can be ensured by minimising the generation of
69 waste and hazardous substances, avoiding disposal practices and maximising the amount of recycled
70 material [7]. The waste hierarchy identified is a crucial strategy for the transition of the EU economy
71 towards a Circular Economy (CE), allowing MSW management to achieve the best environmental
72 performance [8]. According to CE's definition, MSW production should be minimized, maintaining resources
73 as long as possible within the economic cycle [9]. To foster the achievement of a CE condition, a European
74 target on recycling and landfilling rates of at least 65% and 10%, respectively, must be achieved within 2030
75 [10]. Currently, the percentage of landfilled and recycled MSW still remains equal to 23% and 48%,
76 respectively, values far short of the target [11]. According to Chen *et al.* [4], despite the improvements
77 achieved, a continuation of the current waste management trend is insufficient to reduce the pressure
78 generated by MSW management and achieve a CE. In light of these considerations, identifying sustainable
79 solutions for MSW management to support and accelerate the transition towards the achievement of the
80 goals set at the EU level is necessary.

81 Among the actions included in the waste hierarchy (Figure 2), [6] a noticeable category of recovery options
82 is the so-called Waste-to-Energy (WtE), including the treatments to convert MSW into electricity. Although
83 these options are at a lower level (i.e., less preferable) than prevention, reuse and recycling in the waste
84 hierarchy, it can be stated that they are essential to ensure sustainable MSW management and to support
85 the CE transition [12]. WtE treatments, indeed, allow, in this transitional phase, to treat MSW that is not
86 recycled and, simultaneously, to reduce the landfilling rate, consistent with the EU targets and a CE
87 perspective. Once the goals are achieved, these treatments can still be helpful in treating not recyclable
88 materials or perishable waste, avoiding WtE plants' overcapacities. Consistently with these aspects, in the
89 last years, an ever-increasing amount of waste has been processed by adopting WtE treatments [6]. A
90 secondary benefit related to the adoption of the WtE treatment concerns the energy demand of last years.
91 It is estimated that, at the end of this century, the energy demand will be about six times the current one
92 [13] and reach 17 billion tonnes of oil equivalent [14]. In this context, the depletion of fossil fuel reserves

93 and the environmental problems associated with the use of non-renewable sources cannot be neglected
 94 [15]. Kumar and S. R. Samadder [13] estimated that around 1.3 ton $\text{CO}_{2\text{eq}}$ are avoided, using 1 tonne of
 95 MSW for electricity generation. Nevertheless, in EU countries, there is still a strong dependence on fossil
 96 fuels for primary energy production. Nowadays, about 70% of direct energy comes from fossil sources
 97 (Figure 3) [16].



99
 100 **Figure 3.** Share of total primary energy supply in 2018 in EU countries per source. Adapted from [16]

101 Evaluating the potentiality of the existing WtE treatments helps to assess their capability to support and
 102 accelerate the current CE transition. Consistently with the above considerations, the following research
 103 questions (RQ) have arisen:

104 RQ1. What are the key drivers to be investigated to assess the economic convenience of WtE treatments?

105 RQ2. How do the local municipal requirements influence the effectiveness of existing WtE treatments from
 106 an economic perspective?

107 RQ3. Which WtE treatments are available on the market, and what is their potential to support the
 108 transition towards a CE?

109 The present research work's purpose consists of comparing the investment in three different WtE
 110 treatments to identify the best solution to support the current transitional phase towards a CE condition.
 111 To this end, an overall yearly cost analysis was developed by varying local municipal requirements, including
 112 investment, operating, and carbon emissions costs. The overall yearly cost and the revenues, due to energy
 113 sales and tipping fees, allowed to evaluate the profitability of the investment in the plant lifetime to identify
 114 the most sustainable WtE treatment. Specifically, the investigated alternatives were incineration,
 115 gasification and flameless oxy-combustion treatments. The first one is the most widespread, and it is the
 116 oldest in technological terms. The second one is considered the most efficient in terms of recovered energy.

117 The third one is the newest; there are only a few applications at the lab scale, generally adopted for treating
118 low-ranking fuels, coal slurry and industrial wastes [17].

119 A sensitivity analysis was performed to identify the most significant key drivers affecting the convenience
120 of each considered option. The preliminary assessment allowed to identify the most sustainable WtE
121 treatment for MSW management to support the transition phase when applied to the case study of
122 southern Italy's the Metropolitan City of Bari.

123

124 **2. Literature review**

125 Wei Lu et al. [18] analysed incineration as a possible alternative for MSW management and proved its validity
126 despite being an outdated technology. According to the authors, the choice of technology for MSW
127 incineration depends on economic and environmental issues. Generally, the green aspects are affected by
128 the high variability of MSW composition and the lack of reliable control systems. A Life Cycle Assessment
129 (LCA) to evaluate the impact of refuse-derived fuel within the incineration process of the MSW instead of the
130 coal was carried out by Havukainen et al. [19]. The results led to reduce the impact of the main environmental
131 categories (i.e., global warming potential, acidification potential and eutrophication). Panepinto and Zanetti
132 [20] adopted a multi-step approach for the economic and environmental evaluation of an incineration plant
133 in Italy. They considered the capacity of the incinerator plant and possible connections with a district heating
134 network for the use of the heat power produced. At a global and local level, an environmental balance and a
135 cost analysis were carried out to evaluate the efficiency of a plant, including heat and electricity
136 cogeneration. In this case, if, on the one hand, the installation of a cogeneration plant in a heating district
137 minimises the environmental impacts, on the other hand, the configuration that provides only the electricity
138 generation is more convenient from an economic perspective.

139 Similarly, in [21], an LCA was developed to evaluate the environmental impact generated by an incineration
140 plant, including energy recovery in different operating conditions. The research shows that investing in
141 technical improvements is convenient and, therefore, increases the electrical conversion efficiency in the
142 case of a high-size plant. One of the recommended improvements consists of replacing the typical refractory
143 bricks with phase-change material-based bricks in the reactor [22]. It is also shown that the recovery of the
144 bottom ashes helps decrease indices' values in different impact categories [21]. Beylot et al. [23] analysed an
145 LCA related to MSW incineration in France. The study identified a negative indicator for seven of the nine
146 impact categories. In particular, the most significant benefit comes from the cogeneration of heat and
147 electricity as well as from the selective catalytic reduction for NO_x abatement. In 2015, subsystems of the
148 plant were modelled, adopting short-term stochastic planning to manage the energy produced by
149 cogeneration [24]. It is noted that short-term stochastic planning increases net revenues and thermal
150 efficiency instead of determinist short-term planning. In [25], the potential benefits in economic and
151 environmental terms of an MSW management strategy based on the incineration and recycling of MSW for

152 a Brazilian location were assessed. The technique consists in recycling 20% of the collected and selected
153 waste and sending the remaining share to incineration. The results showed the potential of the adopted
154 strategy from economic and environmental perspectives. A similar approach, based on the incineration
155 treatment simulation models, was developed in [26] and [27].

156 Pyrolysis is another MSW treatment recently developed. It is described and detailed in [28], while Wang et
157 al. [29] investigated the environmental feasibility of pyrolysis as an alternative for sustainable MSW
158 management in North Carolina. The environmental impacts of the pyrolysis process were compared with the
159 impact of incineration, anaerobic digestion and landfill. The results proved that fast pyrolysis is the best
160 alternative from an environmental point of view while landfilling is the worst. In [30], the pyrolysis was
161 compared with incineration, gasification and plasma treatment adopting multi-criteria decision-making
162 methods. Li et al. [31] investigated catalytic pyrolysis. They established that if, on the one hand, the use of a
163 catalyst allows a reduction of emissions due to the process, on the other hand, the refrigeration significantly
164 increases the operating treatment costs.

165 Similarly, the performance of catalytic pyrolysis, if compared with thermal pyrolysis, is proved in [32], [33].
166 Wang et al. [34] investigated the potential of pyrolysis, combined with thermal or catalytic cracking, to
167 produce syngas under certain operating conditions. In [35], the effects of moisture content and CaO on the
168 product's composition derived from pyrolysis and syngas' Low Heating Value (LHV) were investigated. Song
169 et al. [36] proposed the addition of iron ore and iron oxide to the treatment as an alternative to improve the
170 efficiency and environmental impact due to the pyrolysis of MSW. According to the authors, iron ore and iron
171 dioxide act as waste pyrolysis catalysts; they improve the efficiency and effectiveness of performance
172 treatment.

173 In the last few years, an increasing interest can be observed in the MSW gasification treatment, which is a
174 valid alternative to other technologies either from a social, economic, and environmental point of view [37].
175 Hameed *et al.* [38] proved the effectiveness of MSW gasification in reducing pollution and maximising the
176 recovery of energy and material. In [39], the effectiveness of the MSW co-gasification with switchgrass was
177 evaluated by considering LHV, the syngas' yield, and the gasifier and tar temperature. Cai et al. [40]
178 investigated the refuse-derived fuels and straw mixtures' co-gasification performance. They identified a
179 positive impact of the synergistic effects on the system's performance at low equivalent ratios (0.1-0.2) and
180 high temperatures (800-900°C). Arena et al. [41] reported a technical analysis of the gasification of a
181 recovered solid fuel obtained from MSW sorting. The report confirmed that adopting the syngas for energy
182 applications was effective. From an economic point of view, the investment can be considered sustainable
183 only if an incentive rate for the energy produced is provided. Kardani et al. [42] modelled the MSW
184 gasification in a fluidised bed gasifier to predict treatment features, such as gas and product LHV, as well as
185 syngas yield. Xu et al. [43] developed a thermodynamic model referring to a real case of MSW gasification.
186 The model allowed to compare the composition of the produced gas using different gasifying agents to

187 identify the best for the treatment's environmental performance improvement. A numerical model to
188 compare different gasifying agents was developed in [44]. In [45], a system based on MSW gasification was
189 proposed to simulate the production of electricity, hydrogen and methanol.

190 Similarly, the performance of a WtE multigeneration system was investigated in [46]. In [47], a biomass-
191 driven cogeneration system was analysed, and the MSW gasification was evaluated. In [48], a thermodynamic
192 model was developed to evaluate the feasibility of MSW gasification in Portugal[49]. The optimal operating
193 temperature of the treatment was identified at 900°C for an equivalent ratio of 0.25. The same approach
194 evaluated the economic convenience of gasifier installation in Brazilian municipalities. The results showed a
195 positive scale-up with increasing the population served, given by reducing the specific costs and increasing
196 the plant's potential [50].

197 Although in previous works, a comparison has already been conducted between different alternatives for
198 producing energy from MSW[51], [52][53], [54], this research work introduces three main novelties. The first
199 consists of evaluating a new unconventional technology without direct emissions, combining the recovery
200 from MSW with the reuse of CO₂ in total compliance with a CE perspective. The second consist of CO₂
201 emissions estimating in the overall yearly cost analysis. The third consists of proposing and testing a new
202 approach to provide a preliminary evaluation of the profitability of an investment in WtE treatment by
203 adopting a more simplified assessment if compared to existing methodologies [49], [50][51], [52]. Therefore,
204 the targets achieved in the present work can be considered a starting point for further analysis in more
205 complex scenarios.

206 **3. Materials and Methods**

207 *3.1 WtE treatments configuration*

208 The configurations considered for incineration and gasification treatments are shown in Figures 4 and 5,
209 respectively. Although CO₂ recovery is also possible in the case of incineration, the most common
210 configurations of the described plants don't include CCS facilities since the treatment required to extract CO₂
211 is not economically sustainable due to low CO₂ concentration and the high presence of contaminant agents.
212 On the contrary, in the case of flameless oxy-combustion, the oxidizing of all combustible material allows
213 obtaining (at zero cost) high concentrations of pure CO₂.

214 Consistent with this consideration, the CO₂ liquefaction process is considered in the plant configuration of
215 the most common flame plants.

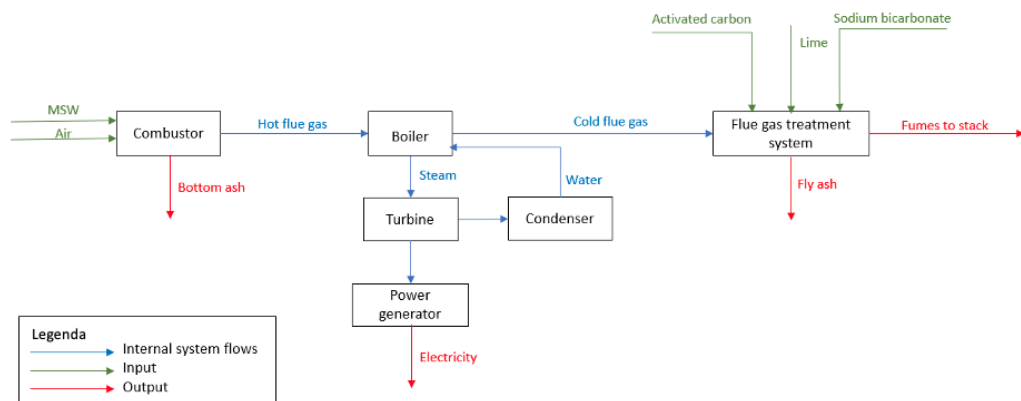
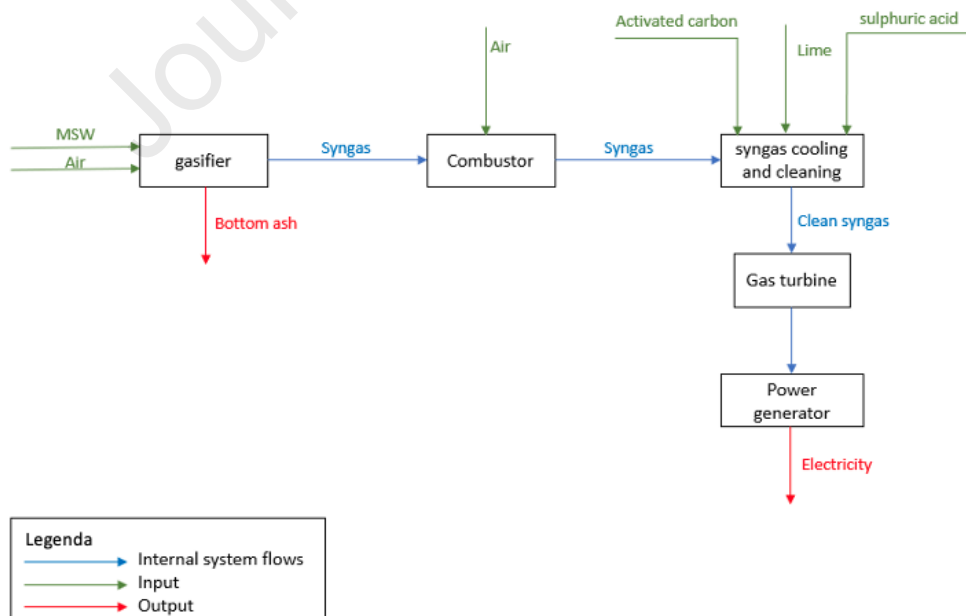


Figure 4. MSW incineration plant configuration

216

217

218 In the incineration treatment (fig. 4), the stored MSW are burnt into the combustor with excess air. Two main
 219 by-products are generated from the combustion, one solid and one gaseous. The solid by-product consists
 220 of unburned products (so-called bottom ash) collected at the bottom of the reactor and then disposed of
 221 outside the system. The gaseous by-product consists of flue gas at a temperature of 1000-1100°C. It is used
 222 to warm up the water in a boiler for steam generation, which is part of a steam cycle of electricity production.
 223 The combustion fumes are conveyed to the flue gas in reactors and bag filters, where specific additives (i.e.,
 224 activated carbon, lime and sodium bicarbonate) are added for dust abatement. Finally, the purified exhausts
 225 are conveyed to the stack and released into the atmosphere.



226

227

Figure 5. MSW gasification plant configuration

228 In the gasification treatment (fig. 4), the MSW is firstly shredded and undergoes a metal removal process.
 229 Then it is fed into a gasifier for degradation at about 900°C, with a sub-stoichiometric percentage of an

230 oxidising agent (e.g., air). Solid slag and a gaseous product, the so-called syngas, are produced by the reaction
 231 in the gasifier. The syngas is burnt in a combustor with air and conveyed to a cleaning system. In the case of
 232 the plant configuration considered in the present work, the purified syngas is used as fuel by a gas turbine
 233 for electricity generation.

234 As shown in fig. 6, the technical oxygen of medium purity (88-94%), the mass of MSW pre-ground mixed in
 235 aqueous solution (i.e., slurry), and the auxiliary fuel (i.e., methane and Very Low Sulfur Fuel Oil (VLSFO)),
 236 enter the combustor. The flameless oxy-combustion is favoured by the combustion chamber's low pressure
 237 and high temperature (around 1300-1500°C) conditions. The MSW oxidation reactions produce two main
 238 types of by-products: solid and gaseous. The solid output consists of vitrified slag produced by the unburnt
 239 material treated with cold water jets in the molten state. The resultant materials are inert pearls with a glassy
 240 structure, so-called vitreous slag (VS), incorporating dangerous substances (not risky to human health and
 241 the environment [53]). The treated VS is potentially adoptable as an additive in concrete mixtures, cement
 242 raw materials, building materials, fluxes, and as a sintering additive [54]. The gaseous output consists of hot
 243 exhausts (around 1300-1500°C) and steam. If mixed in the fumes quencher with the cold fumes recovered
 244 from the blower and cooled at a temperature of 700-800°C, they can be used to produce electricity by a
 245 steam turbine.

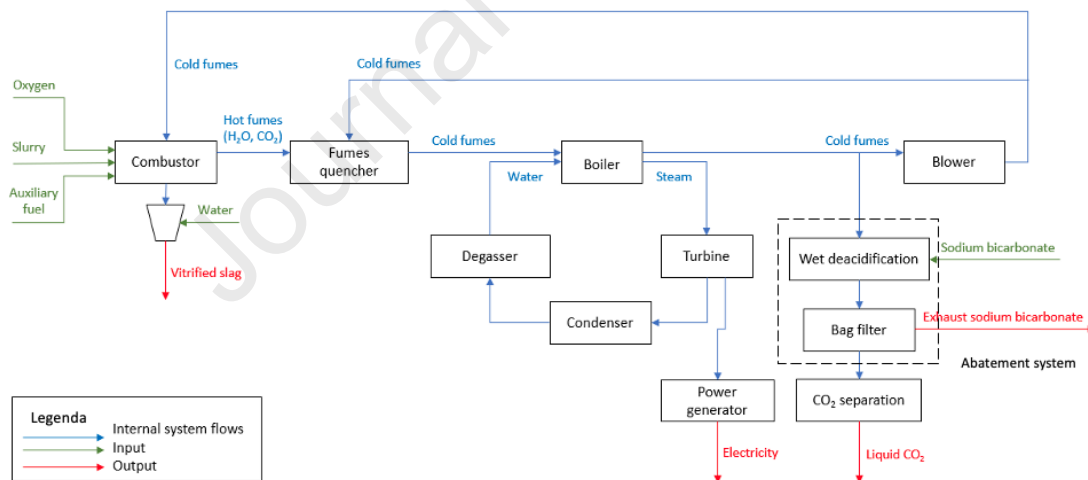


Figure 6. MSW flameless oxy-combustion plant configuration

248 Cold fumes (at a temperature of 200-250°C) in the output of the boiler are conveyed to an abatement system,
 249 including wet deacidification and a bag filter. The dedusted fumes, mainly CO₂, are then treated through a
 250 CO₂ separator and recovered as liquid CO₂ for industrial scopes. It is noteworthy that, for the case in fig. 6,
 251 a zero CO₂ emission process is accomplished. In this WtE treatment, the adoption of technical oxygen as an
 252 oxidizer allows almost all combustible material to be transformed into H₂O and CO₂. This reaction eliminates
 253 the concentration of pollutants in the flue gas [55].

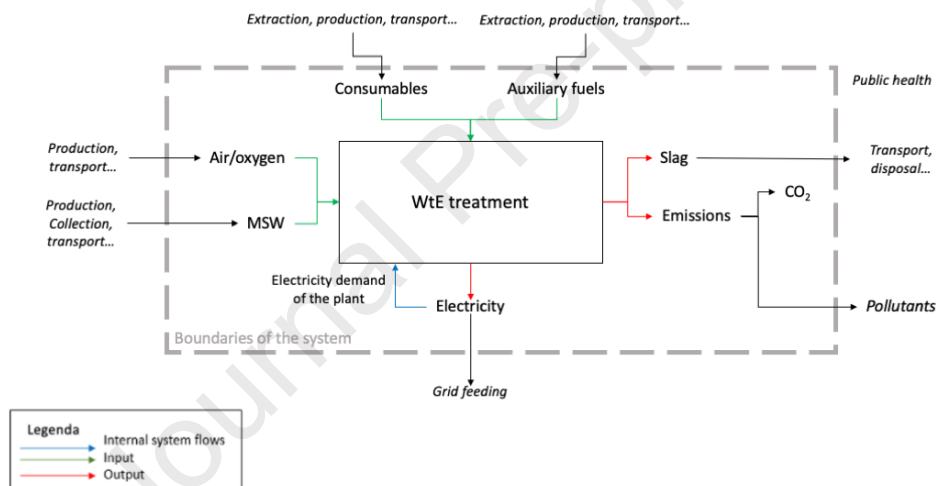
254 Consequently, the obtained flue gas, with a high percentage of CO₂[56], is generally purified, and the CO₂ is
 255 liquefied [57]. This treatment allows the sale of the CO₂ extracted, generating a gain. According to the
 256 assumptions of this work (described in the next section), this kind of revenue is neglected in the economic
 257 evaluation.

258

259 3.2 Assumptions and boundaries systems

260 The proposed cost and investment analysis considers the environmental aspects as an operational cost to
 261 acquire emission rights through carbon pricing [58]. Consistent with this approach, the analysis doesn't
 262 consider the indirect emissions due to the procurement, extraction and transport of raw and auxiliary
 263 materials (fig. 7).

264 Similarly, the evaluations of indirect emissions, as well as the impact on public health due to energy supply,
 265 slag disposal, filtering systems recovery, etc., are out of the boundary of the system considered.



266

267

Figure 7. Systems' boundaries

268

269 Concerning the pollutants in the flue gases, It was considered only CO₂ emissions. Consistent with this
 270 assumption, it can be observed that in the WtE plants considered, the concentration of other pollutants and
 271 particulate matter is strongly reduced by adopting flue gas filtering and purification systems [59], [60], as
 272 shown in plant configurations (Figures 4-6).

273 As far as concerns the revenues from the CO₂ sale in the case of the flameless oxy-combustion plant,
 274 considering the amount of CO₂ produced, the related prices and the processing and storage costs required
 275 to handle the CO₂, the expected profit is negligible if compared to the profit generated from electricity sales
 276 (directly fed into the grid). Consistent with this consideration, only the revenues from the sale of electricity
 277 have been included in the economic assessment.

278 Therefore, the approach proposed assumes a green-field investment on a stand-alone plant that provides to
 279 the decision-maker responsible for the installation and management of the WtE plant a preliminary

280 evaluation on the profitability of the investment in the plant lifetime by varying local municipal requirements,
281 including investment, operating, and carbon emissions costs.

282

283 3.3 WtE cost and investment analysis

284 The cost and investment analysis of the three proposed technologies consists of defining an overall yearly
285 cost ($C_{tot}(q)$) including economic (i.e., investment, operation and maintenance costs) and carbon emissions
286 costs. The MSW annual capacity to be treated (q [tonnes_{MSW}/year]) depends on local municipal requirements.
287 To this concern, a standard size (Q_{std} [tonnes_{MSW}/year]) was set for each investigated WtE treatment. In
288 other words, the Q_{std} -parameter defines the maximum annual capacity to treat MSW of a specific plant. The
289 MSW annual capacity assumed is $Q_{std} = 1E5$ [tonnes_{MSW}/year] for all WtE treatments [61] [62]. In case the
290 yearly amount of MSW to be treated exceeds the given Q_{std} , a significant investment is needed to face the
291 installation of a new thermal utility (C_{ext}). The effect due to possible economies of scale was quantified by
292 assuming a scaling k -coefficient equal to 0.6 [61].

293

294 Table 1 summarises the main items' costs with the corresponding notations.

295

Table 1. List of cost items included in the total cost function

Cost item	Description	Cost type	Notation
Annual investment cost	Investment costs due to acquisition, construction and installation of industrial systems (greenfield project).	Fixed [€/year]	C_{inv}
Investment cost for plant size extension	Investment cost due to thermal facilities acquisition to increase the plant's annual capacity.	Fixed [€/year]	C_{ext}
Maintenance cost	Annual cost for the plant maintenance.	Fixed [€/year]	C_m
Consumables	Cost of additive materials required by the MSW treatments (e.g., oxygen, ammonia, auxiliary fuel, etc.).	Variable [€/tonne _{MSW}]	C_{cons}
Labour	Labour costs to manage the plant operations.	Variable [€/tonne _{MSW}]	C_{lab}
Solid by-product disposal	Cost due to disposal of solid by-products produced by MSW treatments (e.g. slag, ash, baking soda, etc.)	Variable [€/tonne _{MSW}]	C_{SBP}
CO ₂ emissions	Cost due to CO ₂ emitted (i.e., carbon tax).	Variable [€/tonne _{MSW}]	C_{em}

296

297 Fixed costs were evaluated considering the equipment depreciation period, assuming a given available
298 capacity per year. Variable costs were assessed considering the materials needed to treat each tonne of
299 MSW.

300 Assuming the items cost shown in table 1, the WtE treatment $C_{tot}(q)$ ([€/year]) as a function of the annual
301 capacity of the MSW (q) to be treated, is calculated by eq. 1.

$$302 \quad C_{tot}(q) = \alpha + \beta((n-1) \cdot Q_{std}) + C_{ext}(n-1) \sum_{i=1}^{n-1} k^i + \beta(q - (n-1) \cdot Q_{std}) \quad (1)$$

303 with n ($n \in \mathbb{N}$; $n \geq 1$) that identifies the upper integer of the ratio between the MSW annual capacity and
 304 the maximum MSW annual capacity to be treated for a specific plant (eq. 2)

$$305 \quad n = \left\lceil \frac{q}{Q_{std}} \right\rceil \text{ s. t. } q > 0; \quad (2)$$

306 where α and β depend on equations 3 and 4

307

$$308 \quad \alpha = C_{inv} + C_m \text{ [€/year]} \quad (3)$$

$$309 \quad \beta = c_{cons} + c_{lab} + c_{SbP} + c_{em} \text{ [€/tonne}_{MSW}] \quad (4)$$

310 Given C_{inv} and C_m , the other costs are estimated according to equations 5-7.

311

$$312 \quad c_{cons} = q_{cons} p_{cons} \text{ [€/tonne}_{MSW}] \quad (5)$$

$$313 \quad c_{SbP} = q_{SbP} p_{SbP} \text{ [€/tonne}_{MSW}] \quad (6)$$

$$314 \quad c_{em} = q_{em} p_{em} \text{ [€/tonne}_{MSW}] \quad (7)$$

315 where q_{cons} , q_{SbP} , q_{em} , identify the amount of consumables, solid by-products, and CO₂ emissions,
 316 respectively, produced or needed to treat each MSW tonne . Similarly, p_{cons} and p_{SbP} identify the price of
 317 consumables and solid by-products disposal. The p_{em} -parameter represents the economic value assigned to
 318 the local carbon tax.

319 As an extended time period (i.e., twenty years) is considered, and a greenfield investment condition was
 320 assumed, the method of the Net Present Value (NPV)(eq. 8), was adopted to assess the investment
 321 profitability of each WtE treatment. In this case, considering the plant's entire lifetime, the NPV leads to
 322 identifying the investment's capability in WtE treatments to generate money-market liquidity.

$$323 \quad NPV = \sum_{t=0}^N \frac{CF_t}{(1+r)^t} \text{ [€]} \quad (8)$$

324 Where:

325 $t = 0, 1, \dots, N$ [year] is the lifetime of the WtE plant.

326 CF_t [€/year] is the cash flow generated at year t by choosing a WtE alternative.

327 r [%] is the discount rate, i.e., the return value foregone by choosing a WtE alternative.

328 Similarly, the pay-back period time (PBPT) of the investment, corresponding to the time at which the
 329 investment starts to generate monetary liquidity, with regard to the entire investment period, was estimated
 330 as follows (eq. 9):

$$331 \quad PBPT = t \in \{0, 1, \dots, N\} \ni \left| \sum_{t=0}^N \frac{CF_t}{(1+r)^t} = 0 \right. \quad (9)$$

332 For all the considered WtE treatments, the initial investment outlay was assumed to be fully realised at $t=0$.

333 The corresponding yearly costs were estimated according to equation 1.

334 As far as concerned, the revenues generated by the WtE plants, the incomes from electricity sales (paid by
 335 the electricity supplier), and the tipping fee (paid by the municipality to treat MSW) were estimated according
 336 to equations 10 and 11.

$$337 \quad r_e = q_e \cdot p_e \cdot q \text{ [€/year]} \quad (10)$$

338

$$339 \quad r_{t_{fee}} = t_{fee} \cdot q \text{ [€/year]} \quad (11)$$

340 where q_e is the amount of electricity generated per each processed MSW tonne, and t_{fee} is the price paid by
 341 the municipality to treat one tonne of MSW.

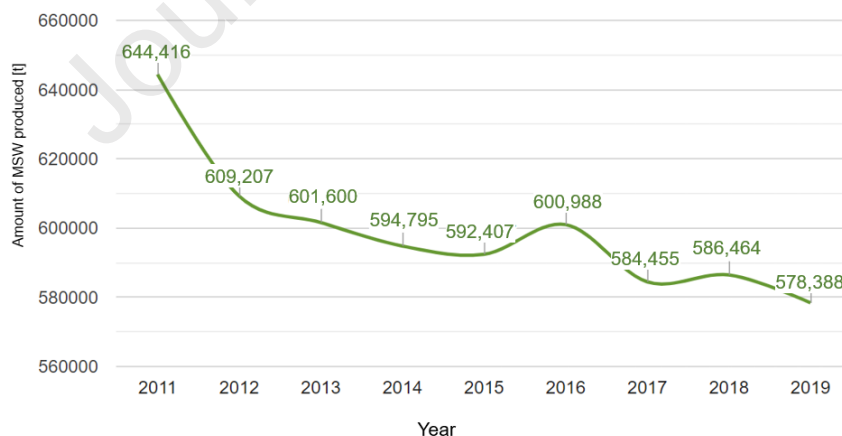
342 4. Case study: the Metropolitan City of Bari, Italy

343 Consistent with the purpose of the present research work, three alternative MSW treatments were
 344 compared to identify the most cost-effective solution for the case of the metropolitan city of Bari, located in
 345 the southern part of Italy.

346

347 4.1 Background of the case study

348 The Metropolitan City of Bari is located in the Apulia region in Southern Italy. In 2019, it had a population of
 349 1.3 million inhabitants. MSW production for the same year was around 580,000 tonnes, with a per capita
 350 production of 463 [kg_{MSW}/(in*year)] [63]. The MSW production from 2011 to 2019 in this area decreased,
 351 from 650,000 to 580,000 tonne/year, showing a reduction of about 10% (fig. 8).

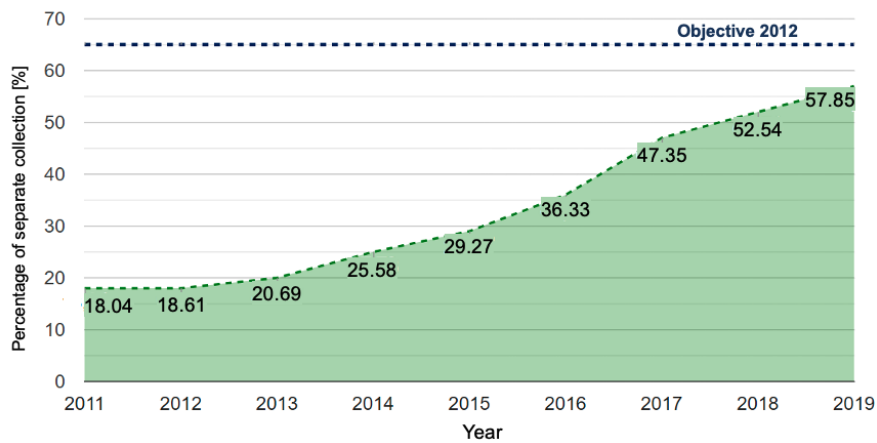


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353

Figure 8. Production of yearly MSW for the Metropolitan City of Bari. Adapted from [63]

354 Considering the target on the percentage of separate collection and recycling of MSW set by the Legislative
 355 Decree no. 152/2006 issued by the Italian Government [64], the Metropolitan City of Bari would ensure a
 356 percentage of separate collection of 65% within 2012, December 31st. In 2019, the rate of separate collection
 357 for the province of Bari was 57.85% [65] (figure 9), which means about 10% less than the expected target. In
 358 2012, about 20% of the separate collection was achieved.



359

360

Figure 9. Actual annual separate collection percentage data for the Metropolitan City of Bari. Adapted from [65]

361 Consistently with Directive 2008/98 of the European Commission, a local target of 55% of waste recycling
 362 within 2025 was set [10]. A share of 47% [67] was currently achieved [65], which is a value far from the
 363 objectives set at the European level. Therefore, the amount of MSW that should be treated by adopting a
 364 WtE solution in the Metropolitan city of Bari is 53% of the total MSW produced, i.e., 306,546 tonnes/year.

365

366 4.2 Numerical assessment for cost and investment analysis

367 The most cost-effective WtE treatment to manage the MSW produced in the Metropolitan City of Bari was
 368 identified by the methodology of Section 3. The cost items corresponding to each of the three WtE
 369 alternatives were assumed according to data available in the scientific literature (Tables 2 and 3). In the case
 370 of most innovative technology (i.e., flameless oxy-combustion), the investment estimation was identified,
 371 assuming an investment cost of 7.69 M€ per each MWe net produced [57], considering that a plant allows
 372 treating 1E5 [tonnesMSW/year] of MSW, produces 10 Mwe [66]. Although, in this research, the flameless
 373 oxy-combustion is considered the most innovative technology, this kind of treatment is largely adopted to
 374 produce electricity and heat from coal and low-ranking fuel [67]. Therefore, no further costs due to
 375 technology immaturity have been considered. The investment costs for incineration and gasification plants
 376 can vary significantly from country to country. Therefore, the average values of the ranges given in [61] have
 377 been considered. The investment costs were estimated considering a useful plant life of twenty years and an
 378 interest rate of 3.5%.

379

Table 2. Yearly investment cost due to acquisition, construction and installation of industrial systems (greenfield project) and
 380 labour costs to manage the plant operations

	Cost	Incineration	Gasification	Flameless oxy-combustion
C_{inv}	M€/year	4.3 [61]	4.95 [61]	5.2 [57]
c_{lab}	€/tonne _{MSW}		8 [68]	

381

382 According to [68], the annual cost for the plant maintenance (C_m) and the investment costs for plant size
 383 extension (C_{ext}) were identified to be used in equations 12 and 13.

$$384 \quad C_m = 0.025 \cdot C_{inv} \quad (12)$$

$$385 \quad C_{ext} = 0.55 \cdot C_{inv} \quad (13)$$

386 **Table 3.** Amount of consumable, solid by-products, emissions and electricity required/produced to treat 1 ton of MSW

Amount required		Incineration	Gasification	Flameless oxy-combustion
q_{cons}	[tonnes]	0.01 [69]	0.03 [69]	0.04 (CH ₄) 0.01 (VLSFO) 0.5625 (O ₂)
q_{sbp}	[tonnes]	0.2 [70]	0.14 [70]	0.25
q_{em}	[tonnes _{CO2}]	0.95 [69]	0.69 [71]	0 [55], [57]
q_e	[MWh]	0.544 [70]	0.685 [70]	0.70 [66]

387

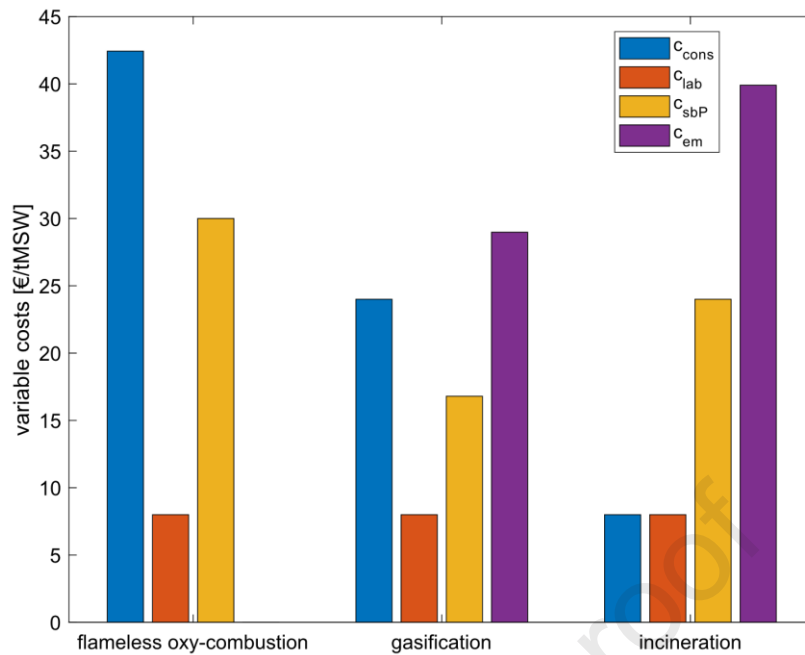
388 Table 4 identifies the economic parameters to be used in equations 5-7. Their values allowed to identify the
 389 overall cost ($C_{tot}(q)$) coming from the treatment of one tonne of MSW for each WtE alternative technology.
 390 In the case of flameless oxy-combustion, the amount of consumables and solid by-products were assumed
 391 in accordance with available experimental data.

392 **Table 4.** The economic value of the parameters considered for the total cost assessment

Parameter	Incineration	Gasification	Flameless oxy-combustion	
p_{cons}	[€/tonne]	800 [72]	800 [72]	300 (CH ₄) 400 (VLSFO) 47 (O ₂)
p_{sbp}	[€/tonne]		120	
p_{em}	[€/tonne _{CO2}]		42 [58]	

393

394 The variable costs associated with one tonne of MSW have been reported in figure 10 for the three WtE
 395 alternatives.



396

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Figure 10. Values of the variable costs for the three considered WtE alternative technologies

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The values assumed in the case study to estimate the NPV in three WtE treatments are summarized in table 5. The evaluation of the investment over a period of twenty years, i.e., a period equal to the useful lifetime of the plants, was assumed. Although each plant could be used for a longer period, including cost due to extraordinary maintenance or revamping activities. Moreover, the time horizon identified depends on the current MSWs management strategies that may be subjected to changes in the long period.

Table 5. Input parameters to investment evaluation

Parameter	Unit	Value
q	[tonne _{MSW} /year]	306,546
N	[year]	20
r	[%]	10%
p_e	[€/MWh]	84 [72]
t_{fee}	[€/tonne _{MSW}]	83 [73]
Income taxes	[%]	35%

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The cash flow statements for the incineration, gasification and flameless oxy-combustion treatment are shown in Appendix B (Table B.1, B.2 and B.3). For each period considered, the value of CF_t , cumulated cash flow (CCF), discounted cash flow (DCF) and cumulated discounted cash flow (CDCF) are provided. According to the performed analysis, the NPV identified for the gasification is equal to 21.7 M€, higher than 19.3 M€ for the flameless oxy-combustion and higher than 66.8 M€ for the incineration. Although the most cost-effective treatment is incineration, looking at the highest NPV value, gasification is the most profitable both from an economical and environmental perspective. This result mainly depends on plant investment and revenue values. Therefore, it is possible to conclude that gasification is the most

413 sustainable solution for the MSW management for the Metropolitan City of Bari, between the WtE
 414 alternatives.

415

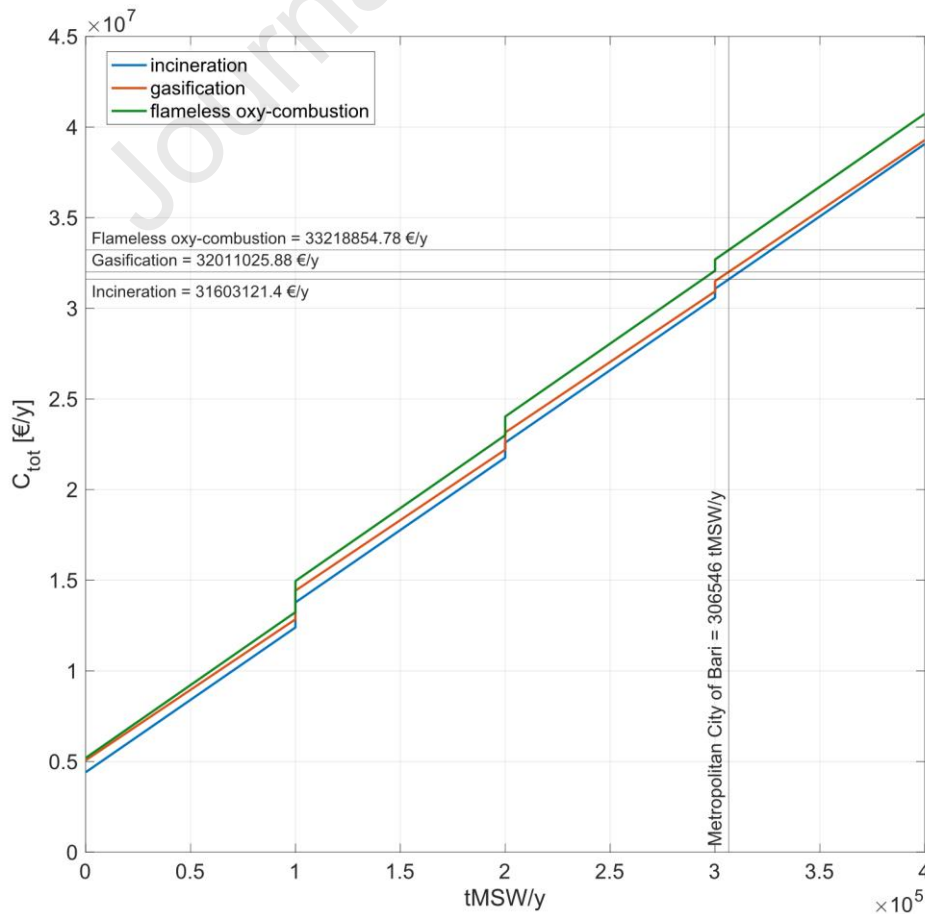
416 5.3 Results and discussions

417 The overall yearly cost of the three WtE treatments depending on the MSW annual capacity to be treated (q)
 418 is shown below (fig. 11). In case no waste is treated, total costs of about 4,410 k€/year, 5,070 k€/year, and
 419 5,200 k€/year were estimated for the incineration, gasification, and flameless oxy-combustion, respectively.
 420 The total cost increases, according to a step function consistent with (eq. 1), when the treated MSW increase.
 421 If the MSW to be treated matches the maximum annual capacity of the plants (i.e., 400,000 tonnes/year), a
 422 cost of about 39.070 M€/year, 39.279 M€/year, 40.735 M€/year was estimated for the incineration,
 423 gasification, and flameless oxy-combustion, respectively. An average increase of 714% of the overall cost was
 424 estimated compared to the zero-waste treatment condition.

425 The lowest costs due to plant extension were identified for incineration. They are lower than 13.2% and
 426 20.9% compared to gasification and flameless oxy-combustion. The effect due to scale economies highlights
 427 a non-linear reduction of plant extension cost with increasing MSW to be treated.

428

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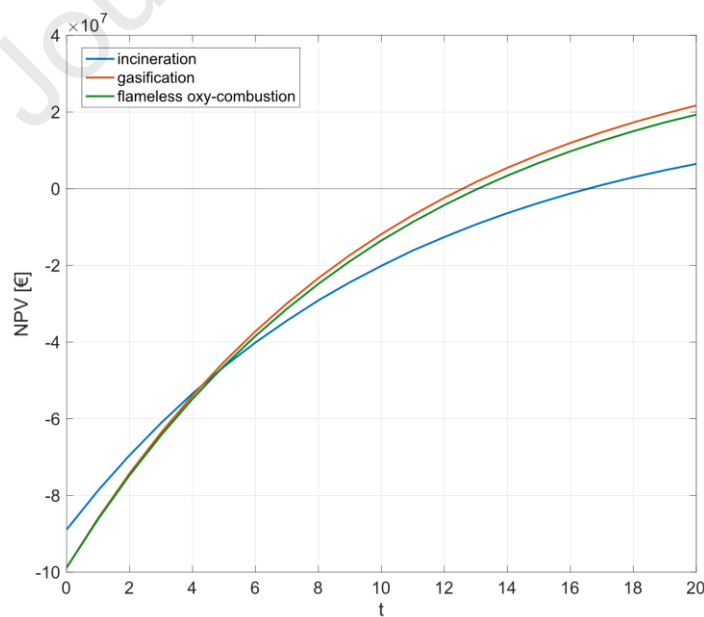
431

Figure 11. Overall yearly cost estimated by changing the annual capacity of the MSW to be treated

432 The comparison among the slopes of the total cost functions represented in fig. 11 shows that the highest
 433 slope is identified for the flameless oxy-combustion case. The slope is related to the variable costs of each
 434 WtE alternative, depending on variable costs supported to manage the WtE plants. In this case, the variable
 435 costs estimated for the flameless oxy-combustion, incineration, and gasification amount to 80.43
 436 €/tonne_{MSW}, 79.9 €/tonne_{MSW}, and 77.78 €/tonne_{MSW}, respectively. Although the variable costs of the
 437 flameless oxy-combustion are independent of the costs due to carbon emissions; the highest consumable
 438 costs lead to increasing the variable costs of this WtE treatment compared to other alternatives (fig. 10). On
 439 the contrary, the highest emission value generated by the incineration treatment (i.e., 0.95
 440 tonnes_{CO2}/tonnes_{MSW}) affected the variable cost of this WtE treatment. From this point of view, although
 441 gasification generates direct emissions, this alternative's lowest consumables cost leads to the lowest
 442 variable costs.

443 In the case of the Metropolitan City of Bari, the amount of MSW yearly produced is 306,546 tonnes.
 444 Therefore, the overall yearly cost estimated for the incineration is lower than gasification and flameless oxy-
 445 combustion by around 1.3% and 5%, respectively. In this case, the revenues, due to energy sales and tipping
 446 fees, allowed to evaluate the profitability of the three investment options in the plant lifetime (fig. 12). The
 447 flameless oxy-combustion technology ensures the highest incomes due to the best efficiency in energy
 448 recovery. Nevertheless, the highest costs related to this WtE treatment reduce the profitability of the
 449 investment compared to gasification (i.e., 12.4%) and incineration (i.e., 64.5%).

450



451

452

Figure 12. NPV of the three WtE alternatives evaluated in a lifetime period

453 The lowest PBPT was estimated for gasification (i.e., 13 years). The flameless oxy-combustion and
 454 incineration treatments show the highest PBPT values, equal to 14 and 17 years, respectively. This means
 455 that the investment in a gasification plant allowed to generate money liquidity over the mid-life of the plant,
 456 while the incineration generates cash at more than 75% of the plant life.

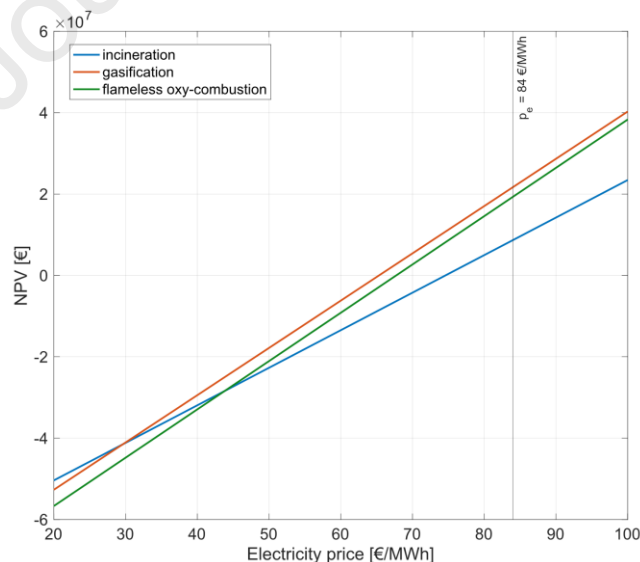
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458 6. Sensitivity analysis

459 A sensitivity analysis was carried out with respect to economic and environmental assessment. In the first
 460 case, the NPV trend was analysed by changing the electricity price for the three WtE treatments (fig. 12). The
 461 investment in the gasification treatment is most profitable from an electricity price of about 30 €/MWh.
 462 Although the flameless oxy-combustion ensures the highest energy production, starting from an electricity
 463 price of about 44 €/MWh, it is more profitable than incineration. For the current electricity price (i.e., 84
 464 €/MWh), gasification is most profitable than other WtE treatments. Nevertheless, the flameless oxy-
 465 combustion could be preferable for higher electricity prices (i.e., greater than 177 €/MWh). The increase of
 466 NPV by varying the p_e -values showed that the NPV of the flameless oxy-combustion increases more than the
 467 NPV of other WtE treatments for a given change of p_e -values. In other words, the electricity price mainly
 468 influences the profitability of the flameless oxy-combustion. This phenomenon depends on the greater
 469 capacity of this WtE treatment to produce electricity.

470

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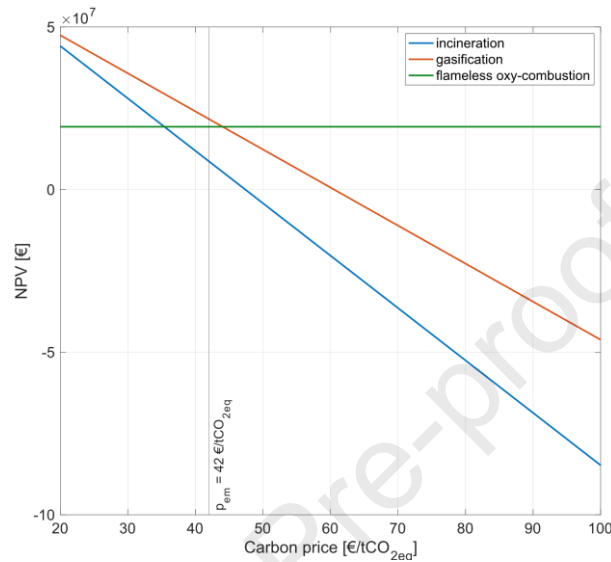
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473

Figure 12. Profitability of the investment by varying the electricity price for each WtE treatment

474 In a second case, the NPV trend was analysed by changing the costs due to carbon emissions produced by
 475 the plant for the three WtE treatments (fig. 13). Gasification is the most sustainable alternative, given the

476 current carbon price [58]. It is more convenient than incineration for each carbon price. Unlike the previous
 477 case, the NPV of incineration and gasification treatment decreases when p_{em} value increases since it
 478 represents a cost item than a revenue. However, the NPV of the flameless oxy-combustion treatment is
 479 independent of the p_{em} variable since it is the only one that does not generate direct emissions into the
 480 atmosphere. It should be more profitable than incineration for a carbon price higher than 44 €/tonnes_{CO₂}.



481
 482 **Figure 13.** Profitability of the investment by varying the carbon price for each WtE treatment

483 The NPV trend was analysed in a third case by changing the tipping fee amount for the three WtE treatments.
 484 In this case, it is observed that the results do not depend on the technology since each alternative's tipping
 485 fee has the same impact.

486 7. Conclusions

487 The scope of the present research work consisted of assessing the investment in three different WtE to
 488 identify the best solution to support the current transitional phase towards a CE condition. Consistent with
 489 this purpose, an overall yearly cost analysis was developed by varying local municipal requirements, including
 490 investment, operating, and carbon emissions costs. The analysed WtE treatments can be considered the most
 491 representative options of conventional, promising and innovative WtE technologies among those available
 492 on the market.

493 The assessment allowed to identify gasification as the best option, at the moment, among the investigated
 494 technologies. Although gasification, compared to incineration, showed the highest variable costs (mainly due
 495 to higher consumable costs), the convenience of this alternative is ensured by high profitability over time
 496 due to high revenues. In this regard, the study showed a strong relationship between the carbon price, the
 497 electricity price and the investment profitability. In particular, a strong dependency on carbon price and NPV
 498 was observed; the flameless oxy-combustion could be preferable for slight price variations and, thus, in the
 499 next future this technology will gain an advantage over all the others when carbon price will increase over

500 the actual price. Another parameter that will increase the oxy-combustion advantage will be the selling of
501 the extracted CO₂ which has been neglected in this study. On the contrary, the tipping fee does not affect
502 the choice among the WtE treatments considered (RQ2).

503 Similarly, it was proved that although the profitability of the three alternatives is strongly related to the MSW
504 amount to be treated, the gasification ensures the highest profitability regardless of local municipal
505 requirements (RQ1). According to the EU targets, WtE treatments are a viable alternative to support the
506 transition phase to a CE condition. In order to identify the potential support offered by the available WtE
507 technologies to this phase (RQ3), an economic analysis was conducted, and three technologies were
508 compared (i.e., incineration, gasification, and *flameless* oxy-combustion). The variables considered for the
509 cost and investment analysis were chosen consistently for this purpose. Revenues from electricity sales (r_e)
510 at the current electricity market price (p_e) were considered, as well as a carbon price, to quantify the adverse
511 effects associated with the emissions generated by the plants (p_{em}). The inclusion of these variables allowed
512 to assess the benefit generated, in the case of each alternative, by electricity production, net of
513 environmental, investment and operating costs and thus to quantify the support offered for achieving a CE
514 condition, reducing the landfilling rate and treating MSW properly. The results achieved showed that the
515 treatment that offers the most support, among those considered, is gasification at the moment. Although
516 this is not the alternative that produces the largest amount of electricity per unit mass of MSW and does not
517 show the lowest total costs (Figure 10), it is the one that shows the best NPV (Figure 11). Moreover, this
518 treatment generates more profit in the shortest time over the plant's useful life (Figure 11). Therefore, in
519 managing this transitional phase, gasification is the alternative that allows keeping a resource within the
520 economic cycle for as long as possible, according to CE's definition, most efficiently, i.e., with the greatest
521 benefits. It is noteworthy that the developed assessment is useful despite the current unstable situation in
522 the energy market. Although in the last twelve months, there has been a 100% increase in the price of
523 electricity for non-household consumers. The priority of preference among the three technologies analyzed
524 does not change since, in all cases, revenue due to electricity sales it was considered.

525 Although the presented approach contributes to investigate the performance of different WtE alternatives,
526 some aspects of the present work could be improved. Future studies and analyses will be performed, also
527 including revenues from heat generation and the costs due to the CO₂ management (e.g., to bury it
528 underground); the recovery options for the solid by-products generated will also be included in the analysis.
529 In addition, the evaluation of transport costs due to MSW collection will be an interesting issue to face. To
530 provide an even more reliable assessment, further analysis of different strategies for MSW management,
531 including issues of end-of-life treatments and the logistics aspects, could be performed.

532

Appendix A. Cash flows Statements of the WtE treatments considered in the case of the Metropolitan City of Bari

533

Table A1. Cash flow statement of the incineration treatment [M€]

534

	t=0	t=1	t=2	t=3	t=4	t=5	t=6	t=7	t=8	t=9	t=10	t=11	t=12	t=13	t=14	t=15	t=16	t=17	t=18	t=19	t=20	
Investment	-88.9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
r_e	0.00	14.0	14.0	14.0	14.0	14.0	14.0	14.0	14.0	14.0	14.0	14.0	14.0	14.0	14.0	14.0	14.0	14.0	14.0	14.0	14.0	14.0
$r_{t\ fee}$	0.00	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4
C_{lab}	0.00	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45
C_m	0.00	-0.111	-0.111	-0.111	-0.111	-0.111	-0.111	-0.111	-0.111	-0.111	-0.111	-0.111	-0.111	-0.111	-0.111	-0.111	-0.111	-0.111	-0.111	-0.111	-0.111	-0.111
C_{cons}	0.00	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45
C_{SHP}	0.00	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36
C_{em}	0.00	-12.2	-12.2	-12.2	-12.2	-12.2	-12.2	-12.2	-12.2	-12.2	-12.2	-12.2	-12.2	-12.2	-12.2	-12.2	-12.2	-12.2	-12.2	-12.2	-12.2	-12.2
Depreciation	0.00	-4.45	-4.45	-4.45	-4.45	-4.45	-4.45	-4.45	-4.45	-4.45	-4.45	-4.45	-4.45	-4.45	-4.45	-4.45	-4.45	-4.45	-4.45	-4.45	-4.45	-4.45
Gross profit	0.00	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4	10.4
Net profit	0.00	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76
Depreciation	0.00	4.45	4.45	4.45	4.45	4.45	4.45	4.45	4.45	4.45	4.45	4.45	4.45	4.45	4.45	4.45	4.45	4.45	4.45	4.45	4.45	4.45
CF	-88.9	11.2	11.2	11.2	11.2	11.2	11.2	11.2	11.2	11.2	11.2	11.2	11.2	11.2	11.2	11.2	11.2	11.2	11.2	11.2	11.2	11.2
CCF	-88.9	-77.7	-66.5	-55.3	-44.1	-32.9	-21.7	-10.5	0.727	11.9	23.1	34.3	45.6	56.8	68	79.2	90.4	102	113	124	135	
DCF	-88.9	10.2	9.26	8.42	7.65	6.96	6.33	5.75	5.23	4.75	4.32	3.9	3.57	3.25	2.95	2.68	2.44	2.22	2.02	1.83	1.67	
CDCF	-88.9	-78.7	-69.5	-61.1	-53.4	-46.4	-40.1	-34.4	-29.1	-24.4	-20.1	-16.1	-12.6	-9.32	-6.37	-3.69	-1.25	0.969	2.98	4.82	6.48	

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Table A2. Cash flow statement of the gasification treatment [M€]

	t=0	t=1	t=2	t=3	t=4	t=5	t=6	t=7	t=8	t=9	t=10	t=11	t=12	t=13	t=14	t=15	t=16	t=17	t=18	t=19	t=20	
Investment	-98.8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
r_e	0.00	17.6	17.6	17.6	17.6	17.6	17.6	17.6	17.6	17.6	17.6	17.6	17.6	17.6	17.6	17.6	17.6	17.6	17.6	17.6	17.6	17.6
$r_{t\text{ fee}}$	0.00	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4
C_{lab}	0.00	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45
C_m	0.00	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124
C_{cons}	0.00	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36	-7.36
C_{SBP}	0.00	-5.15	-5.15	-5.15	-5.15	-5.15	-5.15	-5.15	-5.15	-5.15	-5.15	-5.15	-5.15	-5.15	-5.15	-5.15	-5.15	-5.15	-5.15	-5.15	-5.15	-5.15
C_{em}	0.00	-8.88	-8.88	-8.88	-8.88	-8.88	-8.88	-8.88	-8.88	-8.88	-8.88	-8.88	-8.88	-8.88	-8.88	-8.88	-8.88	-8.88	-8.88	-8.88	-8.88	-8.88
Depreciation	0.00	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94
Gross profit	0.00	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2
Net profit	0.00	9.21	9.21	9.21	9.21	9.21	9.21	9.21	9.21	9.21	9.21	9.21	9.21	9.21	9.21	9.21	9.21	9.21	9.21	9.21	9.21	9.21
Depreciation	0.00	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94
CF	-98.8	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2	14.2
CCF	-98.8	-84.7	-70.5	-56.3	-42.2	-28.00	-13.9	0.271	14.4	28.6	42.7	56.9	71.0	85.2	99.3	114	128	142	156	170	184	
DCF	-98.8	12.9	11.7	10.6	9.67	8.79	7.99	7.26	6.60	6.00	5.46	4.96	4.51	4.10	3.73	3.39	3.08	2.80	2.55	2.31	2.10	
CDCF	-98.8	-85.9	-74.2	-63.6	-53.9	-45.2	-37.2	-29.9	-23.3	-17.3	-11.8	-6.88	-2.37	1.73	5.46	8.85	11.9	14.7	17.3	19.6	21.7	

539 Table A3. Cash flow statement of the flameless oxy-combustion treatment [M€]

	t=0	t=1	t=2	t=3	t=4	t=5	t=6	t=7	t=8	t=9	t=10	t=11	t=12	t=13	t=14	t=15	t=16	t=17	t=18	t=19	t=20	
Investment	-98.8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
r_e	0.00	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18
$r_{t_{fee}}$	0.00	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4	25.4
c_{lab}	0.00	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45	-2.45
C_m	0.00	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124	-0.124
C_{cons}	0.00	-13.0	-13.0	-13.0	-13.0	-13.0	-13.0	-13.0	-13.0	-13.0	-13.0	-13.0	-13.0	-13.0	-13.0	-13.0	-13.0	-13.0	-13.0	-13.0	-13.0	-13.0
C_{shp}	0.00	-9.20	-9.20	-9.20	-9.20	-9.20	-9.20	-9.20	-9.20	-9.20	-9.20	-9.20	-9.20	-9.20	-9.20	-9.20	-9.20	-9.20	-9.20	-9.20	-9.20	-9.20
C_{em}	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Depreciation	0.00	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94	-4.94
Gross profit	0.00	13.7	13.7	13.7	13.7	13.7	13.7	13.7	13.7	13.7	13.7	13.7	13.7	13.7	13.7	13.7	13.7	13.7	13.7	13.7	13.7	13.7
Net profit	0.00	8.94	8.94	8.94	8.94	8.94	8.94	8.94	8.94	8.94	8.94	8.94	8.94	8.94	8.94	8.94	8.94	8.94	8.94	8.94	8.94	8.94
Depreciation	0.00	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94
CF	-98.8	13.9	13.9	13.9	13.9	13.9	13.9	13.9	13.9	13.9	13.9	13.9	13.9	13.9	13.9	13.9	13.9	13.9	13.9	13.9	13.9	13.9
CCF	-98.8	-84.9	-71.1	-57.2	-43.3	-29.4	-15.6	-1.68	12.2	26.1	39.9	53.8	67.7	81.6	95.5	109	123	137	151	165	179	
DCF	-98.8	12.6	11.5	10.4	9.48	8.62	7.83	7.12	6.47	5.88	5.35	4.86	4.42	4.02	3.65	3.32	3.02	2.75	2.50	2.27	2.06	
CDCF	-98.8	-86.2	-74.7	-64.3	-54.8	-46.2	-38.4	-31.3	-24.8	-18.9	-13.5	-8.68	-4.26	-0.244	3.41	6.73	9.75	12.5	15.0	17.3	19.3	

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Declaration of interests

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

The authors declare the following financial interests/personal relationships which may be considered as potential competing interests:

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